

# Changes to heat-treatment of LHC particle-accelerator Nb<sub>3</sub>Sn magnets proposed for optimal results

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## Introduction - Strain Irreversibility Cliff in Nb<sub>3</sub>Sn wires and its challenges

Systematic studies of axial-strain properties of Nb<sub>3</sub>Sn superconducting wires made by the restacked-rod process (RRP<sup>®</sup>) enabled us to discover the *strain irreversibility cliff* (SIC) [1, 2], an abrupt change of the intrinsic irreversible strain limit  $\mathcal{E}_{irr,0}$  as a function of heat-treatment (HT) temperature  $\theta$  for forming the Nb<sub>3</sub>Sn phase. The SIC imposes certain restrictions on HT that are conflicting with those for maintaining the conductor's residual resistivity ratio (*RRR*) above a certain value that ensures stability of magnets against quenching. Hence, SIC poses a real challenge for choosing suitable heat-treatment conditions that can optimize the wire's transport, strain, and thermal properties all at once, especially for large, wind and react, magnet systems.

# Experimental – Measurements of $\mathcal{E}_{irr,0}$ and *RRR* dependences on $\theta$

This work combined studies of strain and *RRR* properties, in close collaboration of ASC-NHMFL, University of Colorado at Boulder, and NIST. We investigated how HT temperature  $\theta$  affects critical-current  $I_c$  vs. axial strain,  $\varepsilon_{irr,0}$  (and SIC), and *RRR* of Nb<sub>3</sub>Sn RRP conductors, and defined the range of  $\theta$  that is suitable to fulfil the competing requirements on multiple parameters for a given Nb<sub>3</sub>Sn RRP conductor design. Temperature  $\theta$  was varied widely, from 599 to 752 °C, for a dwell time at  $\theta$  maintained constant at 48 hours.

# **Results and Discussion**

The study led us to introduce an electro-mechanical stability (EMS) criterion that takes into account both  $\varepsilon_{irr,0}$  and *RRR* requirements. It is a valuable tool to inspect Nb<sub>3</sub>Sn wires *before* their usage in magnets to avoid wasting valuable funds.

When applied to RRP standard-Sn Nb<sub>3</sub>Sn wires, the EMS criterion requires a strikingly narrow HT window that is impractical, especially for massive magnets. In contrast, reduced-Sn wires offer a significantly wider choice of  $\theta$ , not only for ensuring that  $\varepsilon_{irr,0}$  is located at the SIC plateau while  $RRR \ge 150$  (minimum value required for the high-luminosity upgrade of the Large Hadron Collider—HL-LHC), but also for containing the strain-induced irreversible degradation of  $I_c$  beyond  $\varepsilon_{irr,0}$ , as shown in Fig. 1 for HTs varying from 656 to 695 °C.

The HL-LHC project will use reduced-Sn RRP Nb<sub>3</sub>Sn wires, of the same design as the wire presented in Fig. 1. However, HL-LHC current plan is to conduct HTs of dipole and quadrupole magnets at 665 °C. Based on our results, we propose that  $\theta$  for HL-LHC magnets be in the range of 680 to 695 °C instead [2], to ensure that strain-induced irreversible degradation of  $I_c$ , if it occurs during magnet operations, remains limited (Fig. 1).

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## References

- [1] Cheggour, N., et al., Scientific Reports, 8, 13048 (2018).
- [2] Cheggour, N., et al., submitted to Scientific Reports, September 2018.



**Fig. 1:** Comparisons at 4.07 K and 15 T of  $I_c(\varepsilon_0)$  curves for RRP reduced-Sn Nb<sub>3</sub>Sn samples heat-treated for 48 hours at 656, 666, 681, and 695 °C. Samples reacted at 666–695 °C have practically the same  $I_c$  values for any given intrinsic strain  $\varepsilon_0$ , even beyond  $\varepsilon_{irr,0}$ , until the sample reacted at 666 °C starts showing a severe drop of  $I_c$ . This drop is more pronounced for the sample reacted at 656 °C, indicating its gradual evolution with lowering temperature  $\theta$ . The area shaded in gray on the right corresponds to the irreversible strain regime ( $\varepsilon_0 > \varepsilon_{irr,0}$ ).