



## Improved Vortex Pinning and High Field Critical Current Density of Nb<sub>3</sub>Sn Superconductor

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### Introduction

R&D superconducting Nb<sub>3</sub>Sn wires were fabricated at the Applied Superconductivity Center employing new in-house fabricated alloys, in order to investigate the feasibility of wires with enhanced high field properties for future accelerator magnets for the proposed Future Circular Collider (FCC), as well as US-Magnet Development Program (MDP) projects. The target non-Cu critical current density,  $J_c$ , at 4.2 K, 16 T for FCC is 1500 A/mm<sup>2</sup>, value far out of sight of any prior Nb<sub>3</sub>Sn conductor. Previous experiments used Nb-Zr precursor rods surrounded by SnO<sub>2</sub>, which generates ZrO<sub>2</sub> precipitates in the reacted Nb<sub>3</sub>Sn that act as pinning centers. However, the use of Zr leads to a suppression of the irreversibility field  $H_{irr}$ . Here we show results obtained with 2 new ternary alloys, Nb<sub>4</sub>Ta<sub>1</sub>Zr and Nb<sub>4</sub>Ta<sub>1</sub>Hf, and compare them to the commercially used Nb<sub>4</sub>Ta (typical  $\mu_0 H_{irr}$ =23.2 T with  $F_p$  maximum at  $\mu_0 H_{Max}$ =4.7 T). Ta-doping increases  $H_{irr}$  whereas Zr or Hf are intended to enhance pinning force density  $F_p$ .

### Experimental

The samples were measured by VSM in the DC facility at NHMFL in the 35 T magnet in the temperature range between 14 and 1.3 K. From the hysteresis loops, we obtained the layer  $J_c$  and the pinning force density,  $F_p$ .

### Results and Discussion

**Fig.1** compares the layer  $F_p$  curves obtained at 4.2 K while **Fig.2** reports the temperature dependence of  $H_{irr}$ . We observed that adding SnO<sub>2</sub> is detrimental to the (standard) Nb<sub>4</sub>Ta sample, whereas it clearly increases the  $F_p$  maximum, shifting the  $F_p$  peak to 5.3 T for the Nb<sub>4</sub>Ta<sub>1</sub>Zr alloy. However, the Nb<sub>4</sub>Ta<sub>1</sub>Zr+SnO<sub>2</sub> sample has a reduced  $H_{irr}$  (20.9 T at 4.2 K) that limits the  $J_c$  improvement at 16 T. To our surprise, the most striking results were obtained with Nb<sub>4</sub>Ta<sub>1</sub>Hf; with or without SnO<sub>2</sub> the  $F_p$  maximum is more than twice that obtained with the Nb<sub>4</sub>Ta alloy, reaching more than 150 GN/m<sup>3</sup>. Because for Hf additions,  $H_{irr}$ (4.2 K) is 23.1-23.6 T, the  $J_c$ (16T) values are not suppressed with respect to commercial wires and  $H_{irr}$  is actually enhanced when SnO<sub>2</sub> is not used. The net result is that  $J_c$ (16T) more than doubles, achieving the hitherto thought impossible FCC target.

### Conclusions

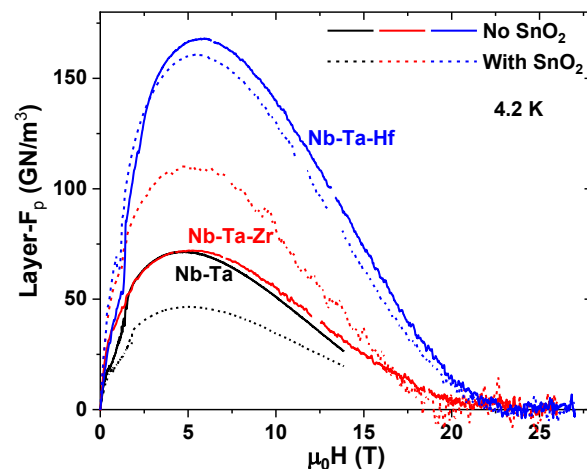
These findings for the Nb-Ta-Hf alloyed Nb<sub>3</sub>Sn wires demonstrate that Nb<sub>3</sub>Sn conductor performance can be greatly improved. We believe that this new alloy can easily be implemented into commercial wires without the difficulty of incorporating SnO<sub>2</sub>. We estimate that a conventional (RRP<sup>®</sup>) wire using Nb-Ta-Hf alloy could attain a non-Cu  $J_c$ (16 T, 4.2 K) of over 2200 A/mm<sup>2</sup>, well above FCC specification.

### Acknowledgements

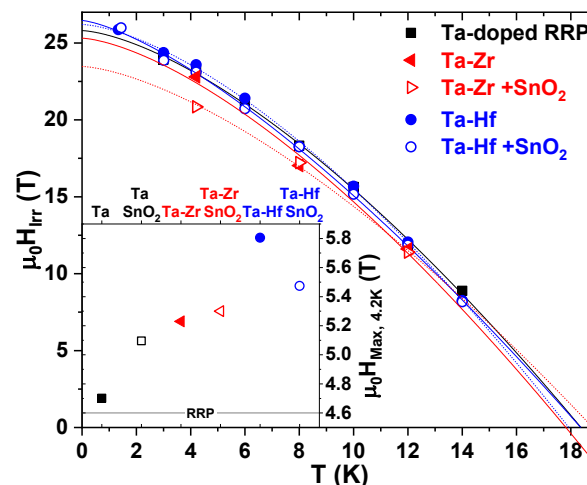
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### References

[1] Balachandran, S., *et al.*, arXiv: 1811.08867 (2018).



**Fig.1**  $F_p$  curves for a in-house quaternary Nb<sub>3</sub>Sn wires showing a significant  $F_p$  enhancement for wires made with Nb-Ta-Zr and Nb-Ta-Hf alloys instead of the standard Nb-Ta.



**Fig.2** Temperature dependence of  $H_{irr}$  of the wires prepared with new alloys compared to a commercial state-of-the-art RRP wire. In the inset the position of the  $F_p$  maximum for all home-made wires.