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Nucleation and growth of discontinuous precipitates in Cu-Ag alloys

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Abstract

To study discontinuous precipitation, which is an important method for strengthening materials, we observed the nucleation and growth of discontinuous precipitates in Cu-Ag alloys using electron backscatter diffraction and scanning transmission electron microscopy. We found that discontinuous precipitation always started with Ag precipitates, which nucleated on Cu grain boundaries. These precipitates then each took the shape of a large, abutted cone that shared a semi-coherent interface with one of the Cu grains, topped by a small spherical cap that shared an incoherent interface with the Cu grain on the opposite side of the boundary. This formation created a difference between the levels of interface energy on each side of boundary. We assume that this difference and boundary curvature together generates the driving force necessary to push grain boundary migration, thus triggering discontinuous precipitation. Because of grain boundary migration, Ag solute was consumed at one side of the grain, which causes a solute difference. The difference produces mainly driving force, pushing the boundaries to migrate forward.

Keywords: Cu-Ag alloys, discontinuous precipitation, nucleation and growth, grain boundary

1 migration

2 **1. Introduction**

3 Deformed Cu-24 wt%Ag alloys are widely used in high-field magnets as conductors
4 because of their high strength and high conductivity [1-5]. The high strength is attributed to a
5 high density of Ag fibers, which evolve from small-sized precipitates in as-cast alloys [1, 6-8].
6 Because of the cost of Ag, many researchers have reduced the Ag content to less than 8 wt%. In
7 such alloys, discontinuous precipitates (DPs) usually occur [3, 9, 10].

8 Discontinuous precipitation has been observed in steels, Mg alloys, Ni alloys, and Cu
9 alloys [11-17]. It is a solid-state reaction that usually has a migrating reaction front, which
10 provides a conduit for fast solute transportation [18]. On both sides of the reaction front, crystal
11 orientations and solute content are different [18, 19]. There are two nucleation mechanisms. The
12 first one was proposed by Tu and Turnbull et al. who studied the DPs in Pb-Sn alloys [20, 21].
13 They assumed that the precipitates that lay on a habit plane and had an orientation relationship
14 with the matrix had the minimum interfacial energy. Then, if the precipitates at grain boundaries
15 lay on a habit plane on one side of grain, they cannot lie on the habit plane on the opposite side
16 because of a tilt angle. This caused the different interfacial energy of the two sides, which
17 formed a driving force to migrate the grain boundaries to remove the high-energy interface. The
18 second one was proposed by Fournelle and Clark who studied discontinuous precipitation in Cu-
19 In alloys [22]. They found that there was no definite habit plane and orientation relationship
20 between In precipitates and Cu matrix. The driving force of initial grain boundaries migration
21 may come from curved boundaries.

22 As far as we know, the nucleation of discontinuous precipitation needs further studies.

23 Some researchers have tried to develop a unified principle to predict the nucleation of DPs from

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3 1 two aspects, i.e., the lattice misfit between precipitates and matrix, and the difference between
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5 2 the atomic radius of solute and matrix, but neither is suitable [18, 23]. The nucleation sites of
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7 3 DPs are also under debate. Many studies have shown that high-angle grain boundaries are
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9 4 nucleation sites, but some studies showed that low-angle grain boundaries also nucleated DPs
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11 5 [18, 24, 25]. Monzen et al. stated that the high-energy grain boundaries were conducive to DPs
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13 6 nucleation and growth because they had high diffusivity [23, 26, 27].
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17 7 In Cu-Ag alloys, many studies have focused on the growth rate and morphology of
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19 8 discontinuous precipitation during steady progress, but there is a lack of research on nucleation
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21 9 itself on an atomic scale [28-31]. Therefore, in this paper, we studied the nucleation and growth
22
23 10 of DPs in Cu-6 wt%Ag and Cu-6wt%Ag-0.05 wt%Sc using Transmission Electron Microscopy
24
25 11 (TEM), atomic resolution Scanning TEM (STEM), and Electron Backscatter Diffraction (EBSD).
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29 12 **2. Materials and methods**

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31 13 We cast Cu-6 wt%Ag and Cu-6wt%Ag-0.05 wt%Sc ingots in an induction furnace at a
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33 14 reduced pressure of 10^{-2} MPa. All the ingots were subjected to solution treatment in two steps:
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35 15 760 °C for 4 h, and 790 °C for 6 h, then quenched in water. Afterwards, we cut several samples
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37 16 from each ingot and aged them at 450 °C for 15 min, 30 min, and 2 h in an argon atmosphere.
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39 17 Most of our data in this paper were from Cu-6 wt%Ag. To generate our findings with different
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41 18 chemistry, we also doped Sc. The role of doped Sc is shown in Ref.14.
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45 19 Ag precipitates were examined with Zeiss 1540 XB field emission scanning electron
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47 20 microscopy (FESEM), JEM-ARM200CF TEM/STEM, and EBSD. The samples for FESEM and
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49 21 EBSD had been subjected to electropolishing in a solution of 30% H_3PO_4 and 70% deionized
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51 22 water with a voltage of 8 V and a current of 4 A. EBSD was performed at 20 kV, a tilt angle of
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1 70°, and a scan step of 1 μm . The samples for TEM/STEM were subjected to argon ion-milling
2 at 5 keV at 7°.

3 **3. Results**

4 Small discrete Ag precipitates (diameter of 7.8 ± 1.4 nm) were found at grain boundaries
5 in Cu-6 wt%Ag samples aged at 450 °C for 15 min (Figs. 1a, 1d). Each of these precipitates was
6 shaped like a large, abutted cone that shared a semi-coherent interface with the Cu grain on one
7 side of the boundary. The cone was topped by a small spherical cap that shared an uncertain type
8 of interface with the Cu grain on the opposite side of the boundary (Figs. 1b, 1c, 1f). Because of
9 resistance from the Zener pinning of the Ag precipitates, some grain boundaries had migrated
10 into the form of a pronounced arc (Figs. 2a, 2b).

11 DPs areas were large when the Cu-6 wt%Ag sample was aged at 450 °C for 30 min (Fig.
12 2c). These areas, which were also observed in Cu-6 wt%Ag-0.05 wt%Sc samples, seem to have
13 been formed between the original boundaries and reaction front, a phenomenon that has also
14 been observed in Nickel-Base Superalloys [32]. EBSD results confirmed that the DPs in these
15 areas had the same crystallographic orientation as the grain behind the reaction front but had a
16 different crystallographic orientation from the grain in front of the reaction front (Fig. 3). The Ag
17 content in the Cu matrix on both sides of the reaction front was considerably different (Fig. 4). In
18 the DP areas, it was only 0.67 ± 0.49 wt%, while in the non-DP areas, it was as high as 6.1 ± 2.1
19 wt%. At the migrating reaction fronts, there were some dark-contrast areas with high Ag content
20 (Fig. 5). We suspected that they were the Ag embryos of DPs. The size of the embryos was so
21 small, no misfit dislocation was required so that Cu/Ag interfaces were fully coherent.

22 Apparently, large lattice distortion occurred in the vicinity of the interfaces. Once the Ag

embryos had grown into DPs, we found semi-coherent interfaces (Figs. 5, 6). In some regions, no lattice distortion was required to accommodate the DP formation (Fig 6).

We investigated the orientation relationship between Cu and Ag and coherency of the interfaces in order to deduce growth orientation and mechanisms of DPs using Cu-6 wt%Ag samples aged at 450 °C for 30 min and 2 h (Figs. 7, 8). The DPs close to the grain boundaries had undefined, irrational growth directions, indicating that the growth was controlled by diffusion (Figs. 8a, 8b). Away from grain boundaries, some DPs grew along [220] direction, with a coherent interface at the front and semi-coherent interfaces on the long sides (imaged at [-112] zone axis, Figs. 7, 8c), where others far from the grain boundaries grew along [3-11] (Figs. 8a, 8b). In twined area of Cu matrix, DPs grew in multiple directions. (Fig. 8d).

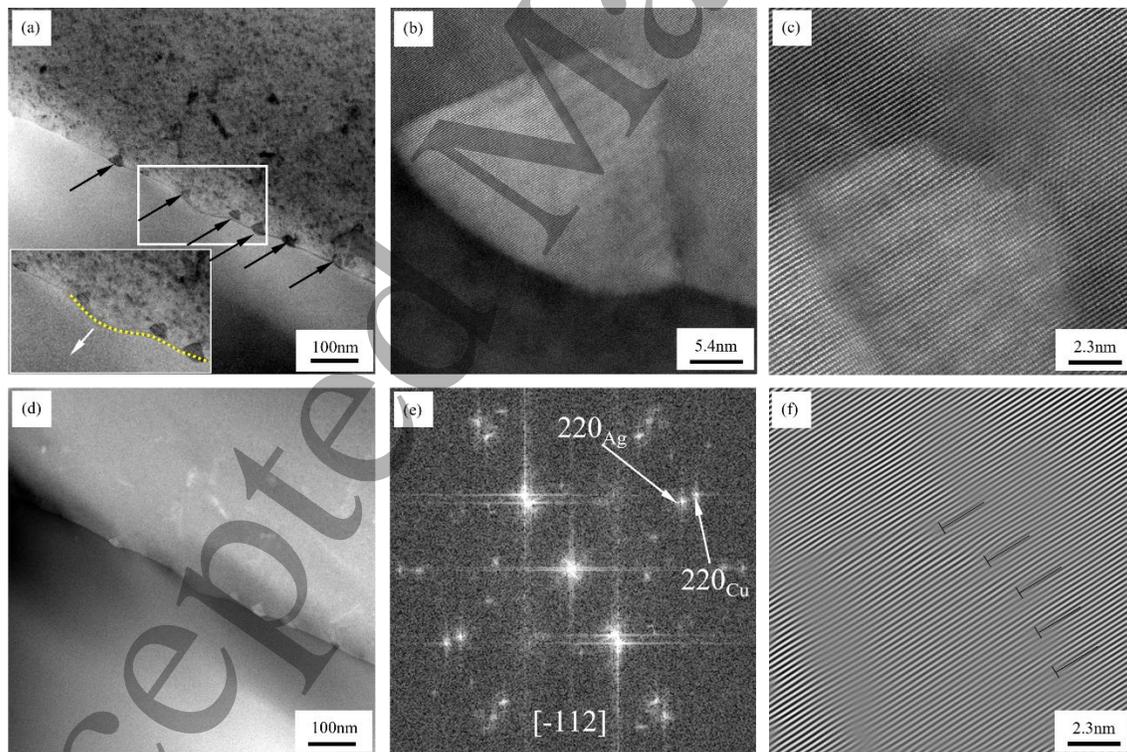
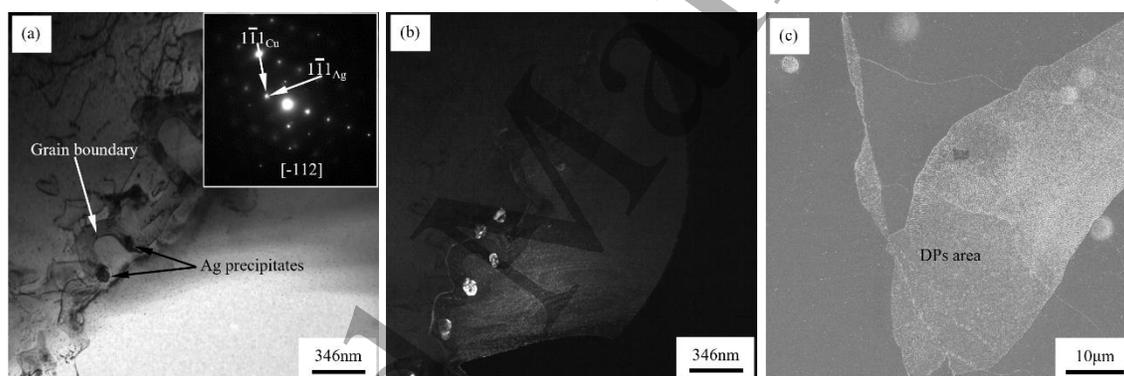
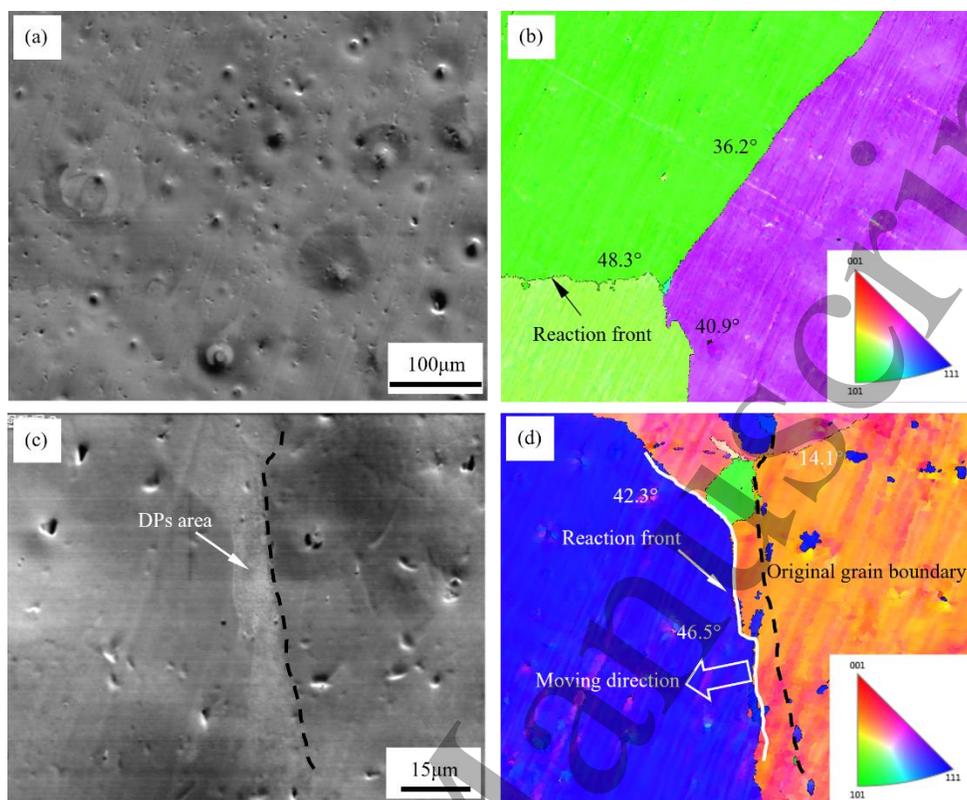


Fig. 1 STEM images showing the nucleation of Ag precipitates on grain boundaries in Cu-6 wt%Ag aged at 450 °C for 15 min. (a, d) Bright-field STEM and high-angle annular dark-field STEM (HAADF-STEM) images of Ag precipitates. Black arrows indicate the Ag precipitates.

1 Inset shows the Ag precipitates and grain boundary at high magnification within a rectangular
 2 outline, and the white arrow indicates the direction of the grain boundary migration. (b)
 3 HAADF-STEM image of Ag precipitate at high magnification. (c) HAADF-STEM image of the
 4 Cu/Ag interface in Fig. b. (e) The corresponding Fast Fourier Transform (FFT) image of Fig. c,
 5 showing the zone axis is $[-112]$, and the Ag precipitate tends to grow along $[110]$ direction. (f)
 6 The corresponding Inverse Fast Fourier Transform (IFFT) image of Fig. c. “T” marks indicate
 7 the positions of misfit dislocations. From the average dislocation distance, the estimated misfit is
 8 around 10.5%. This is smaller than the misfit of bulk materials of Cu and Ag (12.1% [9]), which
 9 indicates that the misfit strain is not released completely by the misfit dislocations.

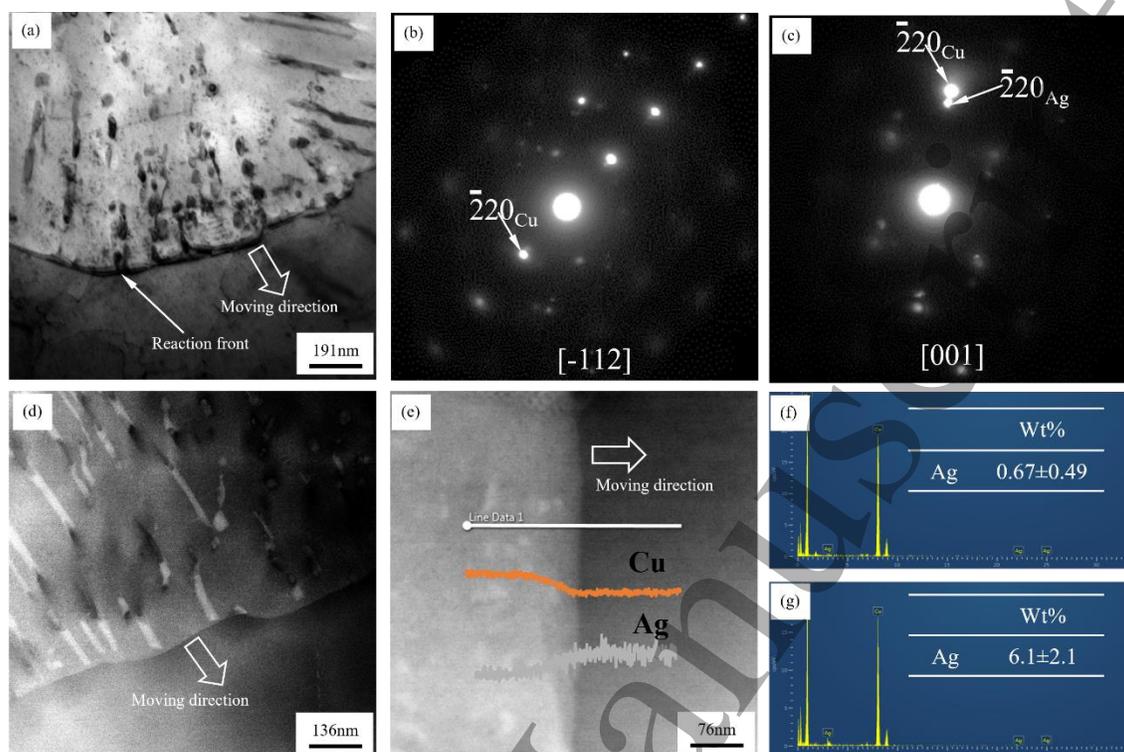


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 11 Fig. 2 TEM/SEM images showing DP areas in samples aged at 450 °C for different times. (a, b)
 12 Bright-field and dark-field TEM images of Ag precipitates in Cu-6 wt%Ag aged for 15 min.
 13 Inset is the selected area diffraction pattern (SADP), showing the zone axis is $[-112]$. (c) SEM
 14 images of the DP areas in Cu-6 wt%Ag aged for 30 min.



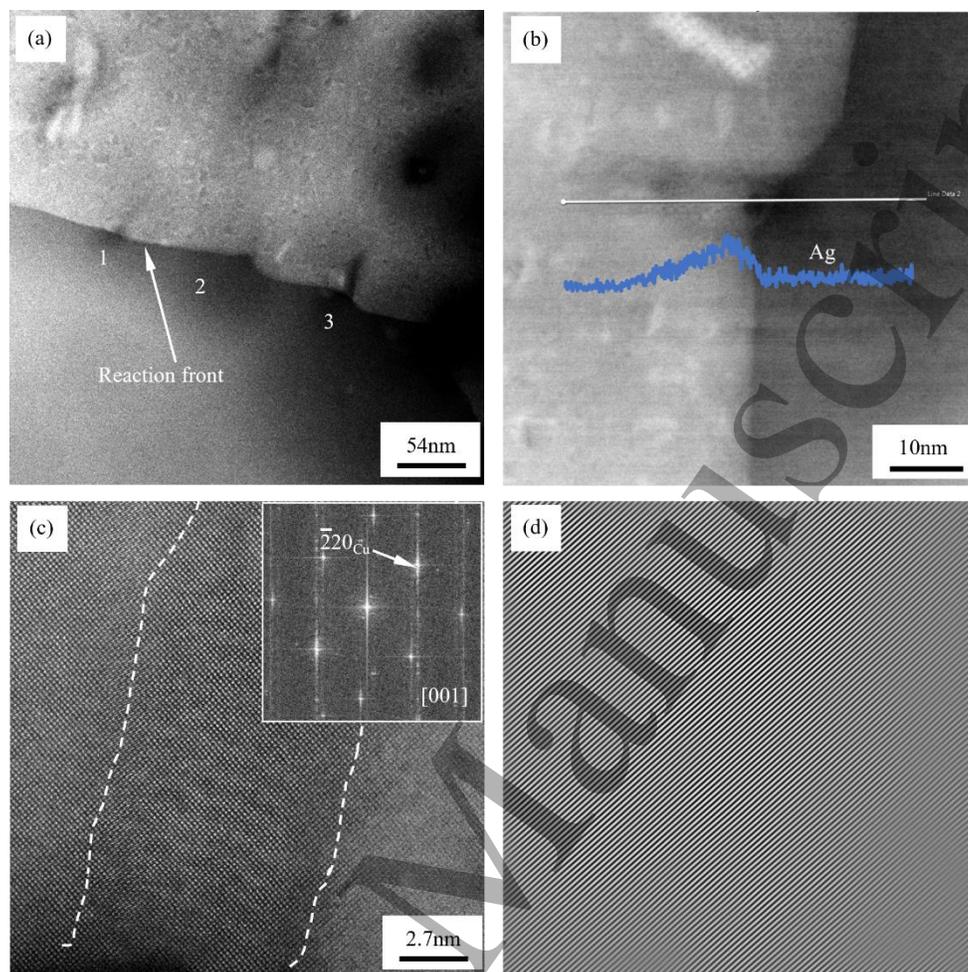
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Fig. 3 SEM/EBSD images showing the crystallographic orientation of DP areas and the grains near the reaction front in Cu-6 wt%Ag-0.05 wt%Sc aged at 450 °C for 30 min. (a, c) SEM images of DP areas. (b, d) Corresponding EBSD images of Figs. a and c.



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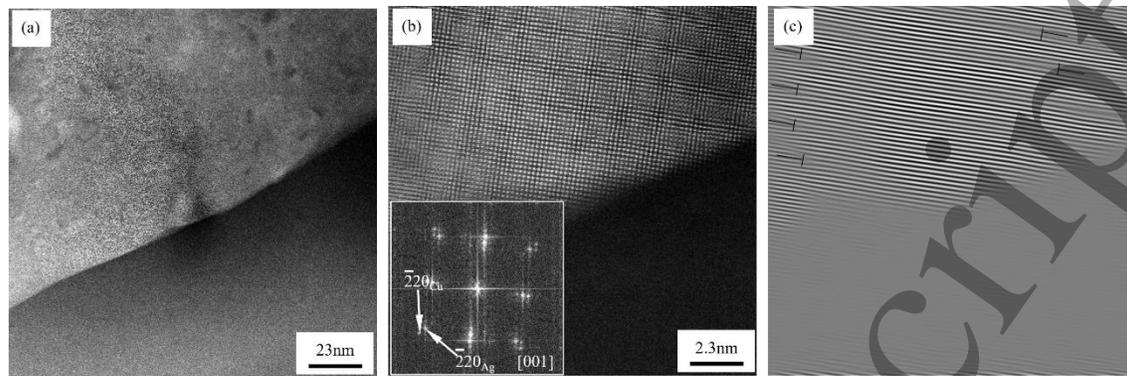
Fig. 4 TEM/STEM images showing the microstructure and element content before and after a reaction front in Cu-6 wt%Ag aged at 450 °C for 30 min. (a) Bright-field TEM image of the reaction front. (b, c) The SADP images of the areas before and after the reaction front, showing the zone axis is close to [-112] and [001], respectively. (d) HAADF-STEM image of DPs. (e) HAADF-STEM image with Ag and Cu composition profile across the reaction front. (f, g) EDS spectrum in areas before and after the reaction front, respectively.



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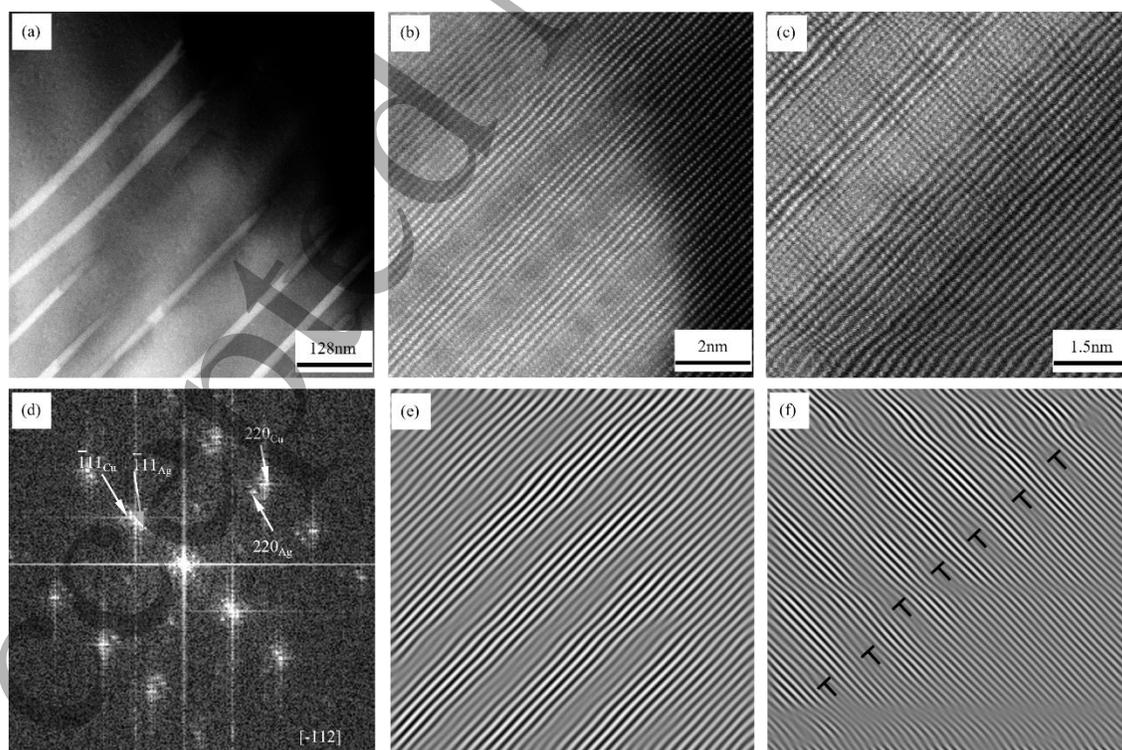
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Fig. 5 HAADF-STEM images showing the embryos of DPs at a reaction front in Cu-6 wt% Ag aged at 450 °C for 30 min. (a) Embryos at the reaction front, which were marked by 1, 2, and 3. (b) The change of Ag content around embryo 2 in Fig. a. (c) High magnification of embryo 2 in Fig. a. Inset is the FFT image, showing the zone axis is [001]. (d) IFFT image of Fig. c showing a coherent Cu/Ag interface.

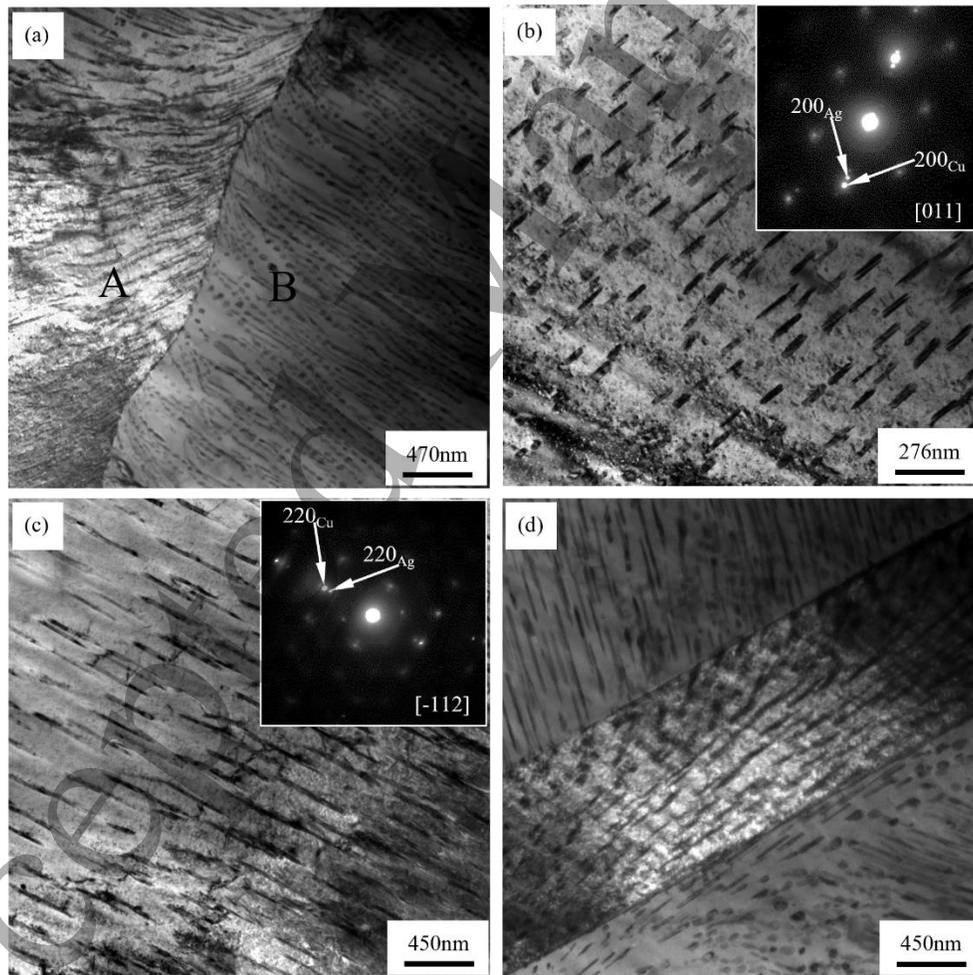


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2 Fig. 6 HAADF-STEM images showing a discontinuous precipitate on a reaction front at Cu-6
3 wt% Ag aged at 450 °C for 30 min. (a) The discontinuous precipitate at the reaction front. (b)
4 High magnification of the precipitate in Fig. a. Inset is the FFT image, showing the zone axis is
5 [001]. (c) IFFT image of the precipitate in Fig. a, showing a semi-coherent interface. “T” marks
6 indicate the positions of misfit dislocations. From the average dislocation distance, the estimated
7 misfit is around 12.5%, which indicates that the misfit strain is released completely by the misfit
8 dislocations.



1 Fig. 7 HAADF-STEM images showing DPs at Cu-6 wt%Ag aged at 450 °C for 30 min. (a) Low
 2 magnification of DPs. (b) High magnification of the Cu/Ag interface at front of a discontinuous
 3 precipitate. (c) High magnification of the Cu/Ag interface along with a discontinuous precipitate.
 4 (d) FFT image of Fig. b, showing the zone axis is $[-112]$. (e) IFFT of Fig. b, showing a coherent
 5 Cu/Ag interface. (f) IFFT of Fig. c, showing a semi-coherent Cu/Ag interface. “T” marks
 6 indicate the positions of misfit dislocations. From the average dislocation distance, the estimated
 7 misfit is around 9.9%, which indicates that the misfit strain is not released completely by the
 8 misfit dislocations.



9
 10 Fig. 8 TEM images showing DPs in Cu-6 wt%Ag aged at 450 °C for 2 h. (a) DPs near a grain
 11 boundary. (b) DPs far away from the grain boundary in grain A. Inset in Fig. b is the SADP

1 image of A grain, showing the zone axis is [011]. (c) DPs far away from a grain boundary. Inset
2 is the SADP image of Fig. c, showing the zone axis is [-112]. (d) DPs, which grow in multiple
3 directions, near twin boundaries.

4 **4. Discussion**

5 In our current work, we found that lattice distortion always occurred in the presence of
6 DPs, whether or not the alloy had been previously doped with Sc. This distortion resulted in both
7 shape anisotropy and internal stress anisotropy [33, 34]. Sc was added to partially suppress DPs
8 in order to understand if our finding can be applied to broader systems.

9 We observed individual formation of nuclei at the grain boundaries similar to that
10 proposed by Tu and Turnbull et al. [20, 21]. All the nuclei in our alloys were Ag particles that
11 had nucleated heterogeneously at Cu grain boundaries. This is similar to what happens in most
12 heterogeneous nucleation, such as Widmannstätten ferrite nucleation in steels [35, 36]. Each
13 shape-anisotropic nucleus had a spherical cap on one side and a cone on the other (Fig. 9).
14 According to heterogeneous nucleation theory, incoherent interfaces usually optimize their shape
15 into spherical caps [37]. Thus, we assumed that the cap-shaped part had an incoherent Cu/Ag
16 interface with a Cu grain on the opposite side of the boundary. Our STEM images showed that
17 each cone-shaped part, on the other hand, had a semi-coherent Cu/Ag interface with a Cu grain
18 on the opposite side of the boundary. Growth on the cone side of a Ag nucleus along a semi-
19 coherent Cu/Ag interface would necessarily be very slow because of the ledge mechanism.
20 Growth on the cap-shaped side, however, would be faster because incoherent interfaces could be
21 expected to have higher mobility and higher energy in the early stages of nucleation. The
22 difference in speed of growth between the two sides meant that the Cu/Ag interfaces moved
23 mainly in one direction. This unidirectional migration caused the growth of Ag in the same

1 direction. The exhaustion of Ag from nearby Cu brought about Cu grain-boundary migration in
 2 the same direction, otherwise known as cooperative growth of Cu and Ag, which indicates that
 3 discontinuous precipitation has occurred.

4 We observed the curved grain boundary that indicated that migration has occurred. Its
 5 energy change (ΔG_g) can be expressed as follows [38]:

$$\Delta G_g = \frac{\gamma_{\text{Cu/Cu}} V_m}{r} \quad (1)$$

6 where $\gamma_{\text{Cu/Cu}}$ is the grain boundary energy in Cu-Ag alloy, V_m is the molar volume, r is the radius
 7 of the grain boundary. At the beginning of grain boundary migration in solution-treated Cu-Ag
 8 samples, $2r$ was as large as the average grain size, which caused a very small G_g . When the
 9 migrating grain boundaries were pinned by Ag nuclei, $2r$ decreased rapidly, thus increasing G_g
 10 and helping the boundaries grow along with the Ag (Figs. 2a, 2c). DPs nucleate easily at high-
 11 angle grain boundaries because these boundaries typically have high $\gamma_{\text{Cu/Cu}}$ [27]. We speculate
 12 that small-sized grains and high grain boundary energy will promote grain boundary migration,
 13 thus triggering discontinuous precipitation.

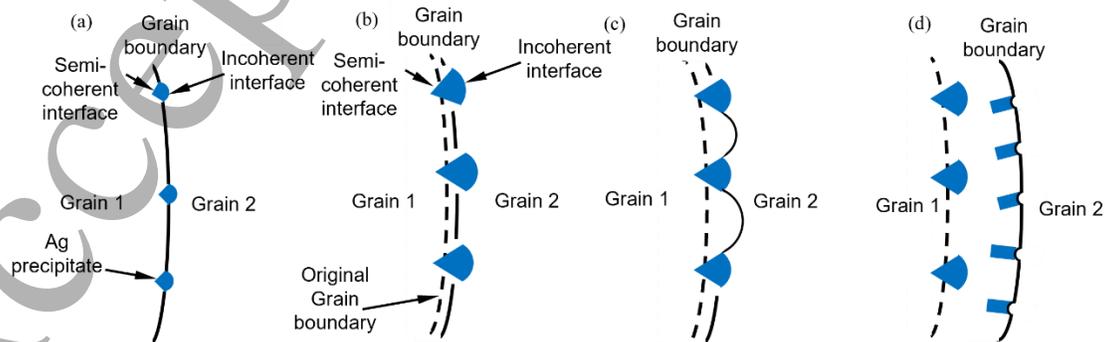
14 Once the Cu grains and the Ag nuclei had established a cooperative growth mode, DPs
 15 began to grow via migrating boundaries (Fig. 4). If one of the phases had had bcc structure, as
 16 previous researchers observed in Cu/Nb, the Kurdjumov-Sachs or Nishiyama-Wasserman
 17 relationship might have occurred [39-41]. At this stage in our study, however, FCC Cu and Ag
 18 established a cube-on-cube orientation relationship. The cooperative growth consumed
 19 supersaturated solid solution and caused energy change (ΔG), which can be expressed as follows
 20 [38]:

$$\Delta G = a\Delta G_0 + b\gamma_{\text{Cu/Ag}} V_m + \frac{\gamma_{\text{Cu/Cu}} V_m}{r} \quad (2)$$

1 where $a\Delta G_0$ is the energy released during discontinuous precipitation, in which a is the fraction
 2 of total energy (ΔG_0), $b\gamma_{\text{Cu/Ag}}$ is the part of the energy that converts to the Cu/Ag interface
 3 energy, in which b is associated with the size and shape of Ag precipitates. We calculated ΔG_0
 4 using follow equation [22, 42]:

$$\Delta G_0 = RT \left[X'_\alpha \ln \frac{X_{\alpha e}}{X'_\alpha} + (1 - X'_\alpha) \ln \frac{(1 - X_{\alpha e})}{(1 - X'_\alpha)} \right] \quad (3)$$

5 where R is the gas constant (8.314 J/K/mol), T is the aging temperature (450 °C in our study),
 6 X'_α is the fraction of Ag in supersaturated Cu (3.68 atom%, from our EDS results, see Fig. 4g),
 7 $X_{\alpha e}$ is the equilibrium solubility of Ag in Cu at 450 °C (0.35 atom%, according to phase diagram
 8 [43]). Our calculation showed that the released energy, ΔG_0 , was -323.7 J/mol. In Eq. 2, b is 2/ S
 9 [44], in which S is the spacing of DPs (77.8 ± 35.6 nm, see Figs. 4a, 4d). $\gamma_{\text{Cu/Ag}}$ is the energy of the
 10 coherent Cu/Ag interface (estimated as 0.23 J/mol by Bacher et al and Bouvalet et al. [45, 46]). r
 11 is the radius of migrating grain boundaries (about 838 nm, see Fig. 4a). Taking a as 0.5, our
 12 calculation showed that ΔG was -112.9 J/mol, where -161.8 J/mol came from the difference
 13 between the Ag solute in different phases, 43.2 J/mol came from the Cu/Ag interfaces, and 5.7
 14 J/mol came from the curved boundaries. This means that when discontinuous precipitation is
 15 steadily proceeding, the greater the solute difference between the two sides of the grain, the
 16 higher the driving energy for grain boundary migration.



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3 Fig. 9 Schematic illustrations of nucleation and growth of DPs in Cu-Ag alloys.
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6 2 **5. Conclusion**

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8 1. When Ag was a solute in Cu-Ag alloys, the nuclei of discontinuous precipitation was
9 always Ag phase, which formed as multiple precipitates at grain boundaries, taking a unique
10 shape of abutted large-sized cone (semi-coherent interface) and small-sized spherical cap
11 (incoherent interface). This unique shape near the interfaces caused the difference of interface
12 energy in two kinds of interfaces, leading to interface growth in one type of interface. The
13 growth of the Ag precipitates drained Ag from surrounding Cu so that new Cu grain migrated
14 with Ag to form discontinuous precipitates.
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18 2. The misfit value between Cu and Ag in DPs was below that of the bulk materials in
19 some cases. At some interfaces, the misfit was zero. This indicated that lattice distortion
20 occurred DPs. The lattice distortion, which was related to the dimension of the interfaces, led to
21 anisotropy in shape, orientation, and stress in the materials. The excessive energy of this lattice
22 distortion provided part of the driving force for formation of DPs.
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26 3. DPs formed between the original boundaries and reaction front. The Ag solute
27 difference on both sides of the reaction front was as large as about 5.4 wt%, which produced
28 driving force for grain boundary migration.
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31 18 **Acknowledgements**

32
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3 **Declaration of competing interest**

4 The authors declare that they have no competing, personal and financial interests in this
5 manuscript.

6 **Data availability statement**

7 All data that support the findings of this study are included within the article (and any
8 supplementary files).

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